

# Do current sources perform to “spec,” as simulated? Hardware for evaluating simulator accuracy

Alistair Boyle

Systems and Computer Engineering, Carleton University, Canada, boyle@sce.carleton.ca

**Abstract:** Ultimately, we aim to test the performance of current sources in SPICE simulation and on biological loads by building representative hardware. We present a preliminary hardware design in this paper.

## 1 Introduction

In this work, we describe our hardware under development (Figure 1), the drive portion of an EIT system, which implements a variety of current source topologies. We aim to use this hardware to take lab measurements and characterize deviations from expected (SPICE simulated) results on resistor or resistor-capacitor (R/RC) phantoms, biological models, and human volunteers. In the following, we describe the preliminary hardware design.

## 2 Back end: digital control and synthesis

The back end of the hardware design consists of a microcontroller (STM32F205, ARM Cortex-M3, STMicroelectronics) supporting USB 2.0 and microSD storage. Power is supplied via USB port and a lithium ion battery. An FPGA (XC6SLX9, Spartan6, Xilinx) provides direct digital synthesis (DDS) connected to a 16-bit digital to analog converter (DAC) (AD5542A, Analog Devices). An integrated DDS/DAC (AD9837, Analog Devices) is also supported. Sync and trigger connectors (SMA) wired to the FPGA support external test and measurement infrastructure.

## 3 Front end: current sources, switching, isolation

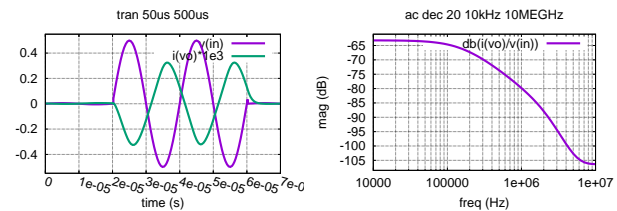
The preliminary design supports current source topologies often selected for EIT designs. These topologies include Howland [1], enhanced Howland [2–5], modified enhanced Howland [6], bipolarity source-sink [1], current conveyor II (CCII) / current feedback opamp [4, 7], and cascode current sources [1]. Except for the last two sources, these current sources are all closely related designs. A repeated common layout is supported for the majority of the current sources so that a variety of designs can be explored with minimal board rework.

To model instrument loads, a transformer-based isolation strategy is implemented at the current source. Beyond the isolation, a switch network models capacitive loads for (effectively) an 8 to 256 electrode array. At the board out-

put, off-board connectors (SMA) enable wiring harness and electrode connections to alternative phantoms and human volunteers.

## 4 Simulated Performance

Performance of an enhanced Howland current source was simulated in Figure 2 (a) transient simulation, and (b) frequency response for an LM741-based design (Texas Instruments) when resistors exhibit a 10% mismatch.



**Figure 2:** Howland current source (left) transient (50 kHz input), and (right) current gain versus frequency simulated in ngspice-30 using an LM741 SPICE model (Texas Instruments)

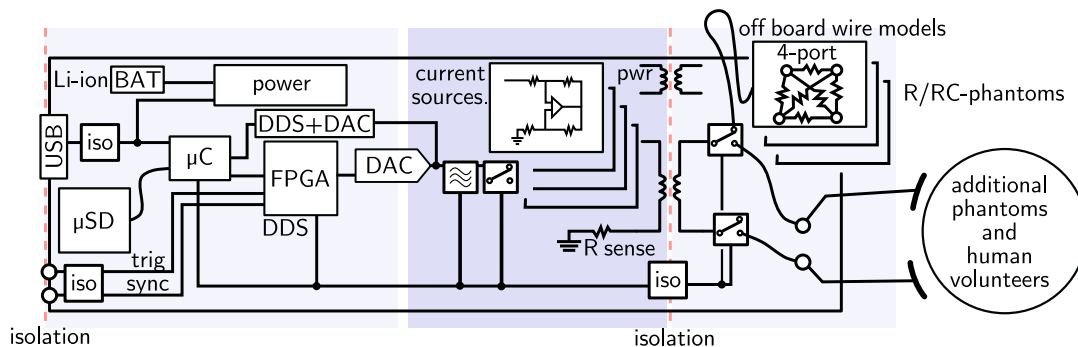
## 5 Conclusions

This work illustrates preliminary work on hardware to be used in validating SPICE simulations of a variety of current source topologies. It is hypothesized that simulations will *not* correlate for biological media due to Cole-Cole type dispersions.

We welcome input on your personal experiences designing EIT hardware and any comments or suggestions you have on our own hardware design.

## References

- [1] Horowitz P, Hill W. *The Art of Electronics*. Cambridge University Press, 3 ed., 2015. ISBN 0521809266
- [2] Cook R, Saulnier G, et al. *IEEE Trans Biomed Eng* **41(8)**:713–722, 1994
- [3] Ross A, Saulnier G, et al. *Physiol Meas* **24(2)**:509–516, 2003
- [4] Holder D (ed.) *Electrical impedance tomography: Methods, history and applications*. IOP Publishing Ltd, 2005. ISBN 0750309520
- [5] Rafiei-Naeini M, McCann H. *Physiol Meas* **29(6)**:S173–S184, 2008
- [6] Maundy B, Elwakil A, et al. *International Journal of Circuit Theory and Applications* **0(0)**:1–10, 2019
- [7] Bragós R, Rosell J, et al. *Physiol Meas* **15(Supplement 2A)**:A91–A99, 1994



**Figure 1:** Block diagram showing the structure of the EIT current source test fixture